

29/4-2013

Tøjning

$$\begin{aligned} \epsilon_{xx} &= \frac{\partial u_x}{\partial x} \\ \epsilon_{yy} &= \frac{\partial u_y}{\partial y} \\ \epsilon_{zz} &= \frac{\partial u_z}{\partial z} \\ \epsilon_{xy} &= \frac{1}{2} \left(\frac{\partial u_x}{\partial y} + \frac{\partial u_y}{\partial x} \right) \\ \epsilon_{xz} &= \frac{1}{2} \left(\frac{\partial u_x}{\partial z} + \frac{\partial u_z}{\partial x} \right) \\ \epsilon_{yz} &= \frac{1}{2} \left(\frac{\partial u_y}{\partial z} + \frac{\partial u_z}{\partial y} \right) \end{aligned}$$

$$\mathbb{E} = \begin{bmatrix} \epsilon_{xx} \\ \epsilon_{yy} \\ \epsilon_{zz} \\ \gamma_{xy} \\ \gamma_{xz} \\ \gamma_{yz} \end{bmatrix} = \begin{bmatrix} \frac{\partial}{\partial x} & 0 & 0 \\ 0 & \frac{\partial}{\partial y} & 0 \\ 0 & 0 & \frac{\partial}{\partial z} \\ \frac{\partial}{\partial y} & \frac{\partial}{\partial x} & 0 \\ \frac{\partial}{\partial z} & \frac{\partial}{\partial x} & 0 \\ 0 & \frac{\partial}{\partial z} & \frac{\partial}{\partial y} \end{bmatrix} \begin{bmatrix} u_x \\ u_y \\ u_z \end{bmatrix}$$

Hooke's law: $\sigma = \mathbb{D} \epsilon$

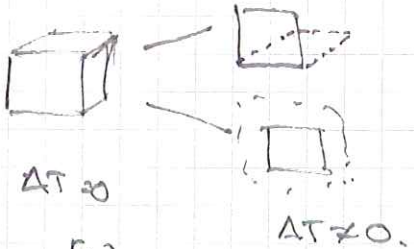
$$\mathbb{D} = \mathbb{D}^1 + \mathbb{D}^2 + \mathbb{D}^3 + \mathbb{D}^4 + \mathbb{D}^5 + \mathbb{D}^6$$

3x1, 3x3, 3x1, 6x1, 6x6, 6x1.

LAS CHARNA:
Berechnungsansatz
mat. modellierung

1D: $W = \frac{1}{2} E (\epsilon^e)^2 > 0$
3D: $W = \frac{1}{2} (\sigma^e)^T D \sigma^e > 0 \Rightarrow D$ pos. det.

Initialtøjning ϵ_0 (ϵ^{AT})
 $\epsilon = \epsilon^e + \epsilon_0$
 $\sigma = D(\epsilon - \epsilon_0) = D(\epsilon - \epsilon^{AT})$

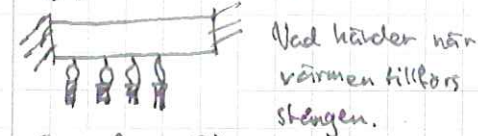


$$\epsilon^{AT} = \begin{bmatrix} 1 \\ 1 \\ 1 \\ 0 \\ 0 \\ 0 \end{bmatrix} \Delta T \otimes \otimes$$

konstitutiv parameter

Sammensætning
Smr: $\nabla \cdot \sigma + b = 0$
Tøjn: $\epsilon = \nabla u$

Konst. samband $\sigma = D(\epsilon - \epsilon^{AT})$
 $\text{div}(\sigma) + b = 0$ $q = D \nabla T$



svag form 3D-elastic:
 $\nabla \cdot \sigma + b = 0 \Rightarrow \begin{cases} \text{div}(\sigma_x) + b_x = 0 & (1) \\ \text{div}(\sigma_y) + b_y = 0 & (2) \\ \text{div}(\sigma_z) + b_z = 0 & (3) \end{cases}$

X-led $\int_{V_x} \text{div}(\sigma_x) dV = \int_{V_x} b_x dV = 0$
Green-Gauss

$$\begin{aligned} \int_{V_x} \sigma_x^T dV &= \int_{V_x} (\nabla u_x)^T \sigma_x + \int_{V_x} b_x dV = 0 \\ \int_{V_x} (\nabla u_x)^T \sigma_x dV &= \int_{V_x} b_x dV \\ \int_{V_x} (\nabla u_x)^T \sigma_x dV &= \int_{V_x} b_x dV \\ \int_{V_x} (\nabla u_x)^T \sigma_x dV &= \int_{V_x} b_x dV \end{aligned}$$

$$\int_{V_x} \sigma_x^T \nabla u_x dV = \int_{V_x} \sigma_x^T \epsilon_x dV + \int_{V_x} \sigma_x^T b_x dV$$

svag form erhalten.

(Wärmeleitung $T = \alpha_1 + \alpha_2 x + \alpha_3 y + \alpha_4 z + \dots$)

$$\begin{cases} u_x = \alpha_1 + \alpha_2 x + \alpha_3 y + \alpha_4 z + \dots \\ u_y = \beta_1 + \beta_2 x + \beta_3 y + \beta_4 z + \dots \\ u_z = \gamma_1 + \gamma_2 x + \gamma_3 y + \gamma_4 z + \dots \end{cases}$$



Approximation (2D)

$u_y = \alpha_1 + \alpha_2 x + \alpha_3 y = N^e a^e$
C-matrixmethode $u_y = N_y^e a^e$

$$U = \begin{bmatrix} u_x \\ u_y \end{bmatrix} = \begin{bmatrix} N_x^1 & 0 & N_x^2 & 0 & N_x^3 & 0 \\ 0 & N_y^1 & 0 & N_y^2 & 0 & N_y^3 \end{bmatrix} \begin{bmatrix} a_1^e \\ a_2^e \\ a_3^e \\ a_4^e \\ a_5^e \\ a_6^e \end{bmatrix}$$

mod 1, mod 2, mod 3.

$\Rightarrow U = N^e a^e$
 $\epsilon = \nabla U = \nabla N^e a^e = B^e a^e$
FE-Formulierung
 $C^T \left(\int_V B^T \sigma dV - \int_S N^T \epsilon ds - \int_V N^T b dV \right) = 0$

lign temperaturerfekt $\sigma = D \epsilon = D \nabla N a = D B a$

$$\int_V B^T D B dV a = \int_S N^T \epsilon ds + \int_V N^T b dV$$

Temperaturerfekt $\sigma = D(\epsilon - \epsilon^{AT})$

$$\int_V B^T D B dV a = \int_V B^T D \epsilon^{AT} dV + \int_S N^T \epsilon ds + \int_V N^T b dV$$

TIPS PROJEKT: plant ϵ .m